## Structure and properties of the directionally Mo-Si-B solidified alloy with the addition of lanthanum

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**Abstract.** The directionally solidified Mo-17,5%Si-8%B-0,5%LaCl<sub>3</sub>(ar.%) alloy was prepared by floating zone method. The microstructure of the alloy consists of Mo<sub>3</sub>Si matrix with predominantly fine-grained inclusions of the Mo<sub>5</sub>SiB<sub>2</sub> (T2) and molybdenum (Mo<sub>ss</sub>) phases and represents the alternation of the two- (Mo<sub>3</sub>Si-T2) and three-phase (Mo<sub>ss</sub>-Mo<sub>3</sub>Si-T2) eutectics with periodic large Mo<sub>ss</sub>.phase activations. The obtained values of integral microhardness and fracture toughness are 9.25±0.5 GPa, 14.32±0.6 MPa m<sup>1/2</sup>, respectively. A solid protective oxide coating was obtained due to 10 hours air holding at 1030°C.

Keywords: floating zone method, eutectic, oxidation, borosilicate coat.

**Introduction.** Last years the scientific interest to Mo-Si-B alloys, which can become potential substitutes for nickel superalloys for manufacturing of turbine blades and other high-temperature units, was considerably increased, because they have higher operating temperatures and can significantly increase of energy efficiency of gas turbine engines.

Literature review. The alloys of Mo-Si-B system consisting of a molybdenum solid solution (Moss) and two other intermediate Mo<sub>5</sub>SiB<sub>2</sub> (T2) and Mo<sub>3</sub>Si (A15) phases uniformly distributed in the microstructure show attractive mechanical and oxidizing properties at temperatures above 1100 ° C [1]. This system became the subject of close attention, since the temperature of application may exceed the temperature of the application of super-alloys based on nickel [2]. The Mo-Si-B alloys has excellent oxidation resistance above 1100 ° C, due to the formation of a low viscose borosilicate coating that covers the surface of the material and provides protection against further oxidation [3]. However, alloys of the Mo-Si-B system show a low resistance to oxidation in the range 650-900 °C [4] when the borosilicate coating is not formed yet, which causes the formation and evaporation of MoO<sub>3</sub>. Recent studies [5,6] have shown that the addition of rare earth elements improves both the oxidation resistance of such materials over a wide range of temperatures and their mechanical characteristics.

The current task is to prepare the alloy of Mo-Si-B system with optimal microstructure, mechanical properties and resistance to oxidation [1,7]. Using of directional crystallization allows to efficient control of structure and properties due to variation of technological parameters of growing, which enables to control both oxidative and mechanical properties [8].

**Objective.** Therefore, the purpose of this work was to study the influence of addition of lanthanum on the structure and properties of directionally solidified Mo-17.5 (at.%) Si-8 (at.%) B alloy.

**Experimental details.** Directionally solidified Mo-17,5 at.% Si-8 at.% B alloy with an admixture of 0.5 atomic % of LaCl<sub>3</sub> was prepared by floating zone melting of nonsintered powdered rods. The molybdenum, silicon, boron and lanthanum chloride powders with a purity of 99.95%, 99.9%, 98%, and 99%, respectively, were used as starting materials. The average particle size of molybdenum powder was 3.4  $\mu$ m, silicon powder - 1.2  $\mu$ m, boron powder - 0.5  $\mu$ m, lanthanum chloride powder - 2  $\mu$ m. A mixture of powders was prepared by 10-fold wiping through a sieve with cells measuring 50 microns. As a plasticizer the 2.5% aqueous solution of polyvinyl alcohol was used. Long-length billets with a diameter of 10 mm and a length of 145 mm were pressed on a hydraulic press under a pressure of 50 MPa and dried in a vacuum oven at 100°C. Zone melting of samples was carried out in the high-frequency "Crystal 206" machine with induction heater.

The microstructure of the samples was studied using a scanning electron microscope (SEM) "SELMI PEM 106". X-ray diffraction analysis was carried out at the "Rigaku Ultima IV" diffractometer. Micromechanical properties were investigated using the microhardness tester MHV-1000. Studies on oxidation resistance were conducted on a Q-1000 derivatograph to 1030 °C with a heating rate of 20 °C/min on air atmosphere for 10 hours.

**Results and discussion** .The investigation of the microstructure of the directionally solidified Mo-17,5Si-8B-0,5LaCl<sub>3</sub> alloy by SEM showed the presence of three phases:  $Mo_3Si$  gray matrix, mainly small dark gray inclusions of  $Mo_5SiB_2$  (T2) and light particles of a solid solution of molybdenum (Moss) (Fig. 1).



Fig. 1. Microstructure of the Mo-17,5Si- 8B-0,5LaCl<sub>3</sub> alloy: a - x500; b - x250

Thus, the microstructure of the observed material is represented by the alternation of the two ( $Mo_3Si-T2$ ) and three-phase ( $Mo_{ss}-Mo_3Si-T2$ ) eutectic with periodic large inclusions of the  $Mo_{ss}$  phase.

The structure in the center of the sample is distributed rather uniformly, but closer to the periphery there is a conventional border of division, after which the structure has a clearly directional character. The molybdenum solid solution and the T2 phase were crystallized in the material as dendritic crystals. It is observed the tendency of the dendritic branches to the side borders of the sample due to the temperature gradient between the center and the edge of the crystallization front. The exclusive feature of the alloy is the fine-grained nature of the structure (Fig 2).



Fig. 2. Macrostructure of the Mo-17,5Si- 8B-0,5LaCl<sub>3</sub> alloy from the center to the edge of the sample

The X-ray phase analysis of the Mo-17,5Si- 8B-0,5LaCl<sub>3</sub> alloy confirmed the presence of only 3 phases: molybdenum solid solution and both intermetallic phases: Mo<sub>3</sub>Si and Mo<sub>5</sub>SiB<sub>2</sub> (Fig. 3).



Fig. 3. X-ray diffractogram of the Mo-17,5Si- 8B-0,5LaCl<sub>3</sub> alloy

By the Vickers indentation method the values of integral microhardness and fracture toughness of the alloy as  $9,25\pm0.5$  GPa and  $14,32\pm0.6$  MPa m<sup>1/2</sup> were obtained. Such values of the micromechanical properties exceed the values previously obtained for the Mo-17,5Si-8B alloy [8] and are explained by a uniform fine-grained eutectic structure of the prepared material.

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Fig. 4. Macrostructure of the alloy Mo-17,5Si- 8B-0,5LaCl3 after oxidation.

The investigation of oxidation behavior of the material showed that the sample exposure for 10 hours at a temperature of 1030 °C on air atmosphere leads to the formation of the dense protective coating (Fig. 4). Three characteristic zones are distinguished on the microstructure: the oxide layer, the transition zone and the main material. According to [3], the protective layer is a borosilicate SiO<sub>2</sub>-B<sub>2</sub>O<sub>3</sub> coating and the transition zone consists of two phases: MoO<sub>2</sub> and Mo grains. The formation of MoO<sub>2</sub> and Mo grains may indicate a low partial pressure of oxygen at the interface between the oxide layer and the transition zone, showing the presence of a stable protective coating in the resulting material.

**Conclusions.** Thus, the directionally solidified eutectic alloy is prepared by floating zone melting of nonsintered powdered rods of Mo-17,5Si-8B-0,5LaCl<sub>3</sub>. The microstructure of the alloy consists of the Mo<sub>3</sub>Si matrix with predominantly fine-grained inclusions of the Mo<sub>5</sub>SiB<sub>2</sub> (T2) and molybdenum solid solution (Moss) phases and represents the alternation of the two- (Mo<sub>3</sub>Si-T2) and three-phase (Moss-Mo3Si-T2) eutectic with periodic large Moss phase activations. The values of integral microhardness and fracture toughness of 9.25±0.5 GPa and 14.32 $\pm$ 0.6 MPa m<sup>1/2</sup>, respectively, exceed the value for non-alloyed Mo-17,5Si-8B alloy. The investigation of oxidation behavior of the material showed that the sample exposure for 10 hours at a temperature of 1030 °C on air atmosphere leads to the formation of the dense protective coating.

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